

MEBT Cavities

16 January 2013

RAL

MEBT Re-bunching cavity engineering design:

Different cavities for the MEBT have been considered

The objective is to keep the target frequency 324 MHz and high efficiency value while allowing space for ports on the circumference of the cavities.



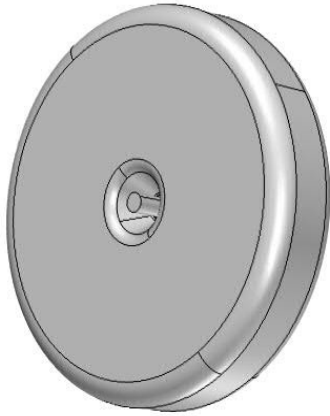
$F=324$
MHz

$Q=28284$

Model 51

Baseline model with no ports

$f=315.68$ MHz, $Q=27963$

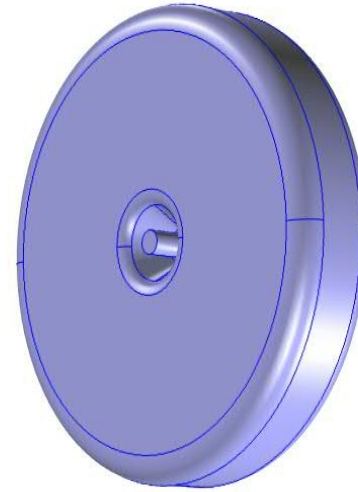


Model_71

ReBunchingCavity7_R=36mm_D=606mm
_InnerVolume

**To investigate effect of 36mm
internal radius allowing for CF40
flange**

$f=321.17$ MHz, $Q=27900$

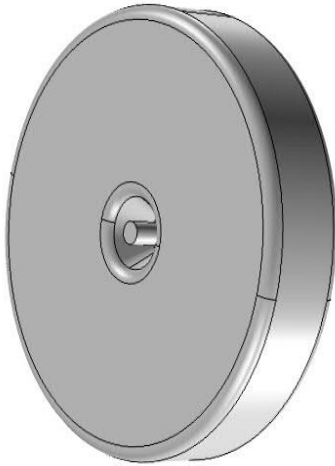


Model_72

ReBunchingCavity7_R=36mm_D=591mm
_InnerVolume

**Reduced diameter to bring
frequency up**

f=321.85 MHz, Q=27496



Mode_73

ReBunchingCavity7_R=20mm_D=584mm_InnerVolume

**To investigate effect of 20 mm
internal radius allowing for CF75
flange**

f=324.17 MHz, Q=27861

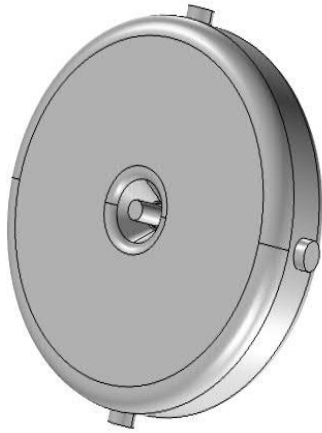


Mode_74

ReBunchingCavity7_R=36mm_D=583mm_InnerVolume

**To bring the frequency to
324MHz**

$f=324.06$ MHz , $Q=27745$

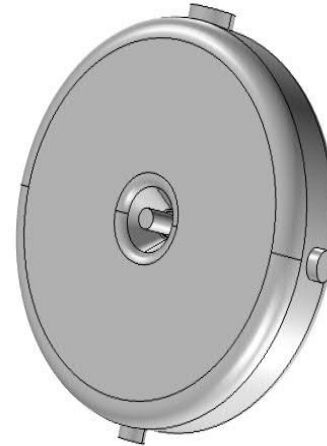


Model_75

ReBunchingCavity7_R=36mm_D=583mm
_Ports=45mm

**Model 74 with 4 diameter 45mm
ports**

$f=323.97$ MHz, $Q=27712$



Model_76

ReBunchingCavity7_R=36mm_D=583m
m_Port=77mm

**Model 75 with 1 port enlarged to
77mm diameter**

No cavity shows drastic drop in Q value

| Model | Inner radius | Frequency | Q | Q change % | Diameter | Max port size | Purpose |
|-------|--------------|---------------|--------------|-------------------|----------|---------------|--|
| | (mm) | (MHz) | | (w.r.t. Model 51) | (mm) | diam (mm) | |
| 51 | 72 | 323.95 | 28284 | 0 | 606 | 0 | Baseline model with no ports |
| 71 | 36 | 315.68 | 27963 | 1.15 | 606 | 45 | To investigate effect of 36mm internal radius |
| 72 | 36 | 321.17 | 27900 | 1.38 | 591 | 45 | Reduced diameter to bring frequency up |
| 73 | 20 | 321.85 | 27496 | 2.87 | 584 | 77 | To investigate effect of 20mm internal radius |
| 74 | 36 | 324.17 | 27861 | 1.52 | 583 | 45 | To bring the frequency to 324MHz |
| 75 | 36 | 324.06 | 27745 | 1.94 | 583 | 45 | Model 74 with 4 diameter 45mm ports |
| 76 | 36 | 323.97 | 27712 | 2.06 | 583 | 3*45+1*77 | Model 75 with 1 port enlarged to 77mm diameter |

MEBT Cavities Power and Voltage (Normalization)

| Parameter | SF | HSFF | MWS |
|------------------------|--------|---------|---------|
| Frequency (MHz) | 324.0 | 323.961 | 324.103 |
| Q | 27815 | 27812 | 28150 |
| Shunt Impedance(M Ohm) | 6.0427 | 5.987 | 5.984 |
| Power Dissipation (kW) | 11.26 | 10.32 | 11.13 |
| Stored Energy(J) | 0.154 | 0.141 | 0.154 |
| Axial Voltage (kV) | 260.85 | 248.62 | 258.06 |
| Effective Voltage (kV) | 160.0 | 152.5 | 158.3 |

**Note that
 $R/Q=217.24$**

COMSOL Simulation and Normalization

$$F=3.2395e8+5729.59i \text{ (Hz)}$$

$$Q=28284$$

$$V=18.19 \text{ (v)}$$

$$W=7.4888 \times 10^{-10} \text{ (J)}$$

$$R/Q=V^2/\omega W=217.26$$

$$R=6.144981 \text{ (M}\Omega\text{)}$$

It's obvious that if we consider $W=0.154 \text{ (J)}$ then through $V^2=(R/Q)\omega W$ we will have: $V=260 \text{ (kV)}$

Which is consistent with the other software results.

The results with COMSOL showed comparable values with the other software results. It remains how the value of 260 kV relates to the values used in GPT for particle tracking.

Estimate for our RF Amplifiers specifications from GPT

| Frequency(MHz) | <i>Old lattice (scheme A)</i> | <i>New lattice (scheme Z+1)</i> |
|-----------------------|----------------------------------|---------------------------------------|
| | 324 | 324 |
| Number of Cavities | 4 | 3 |
| Voltage(kV) | $V_1=94.600$ | $V_1=94.600$ |
| | $V_2=81.700$ | $V^2=86.000$ |
| | $V_3=68.800$ | $V_3=81.700$ |
| | $V_4=53.750$ | |
| Shunt impedance(MOhm) | $R=6.04275$ (Ciprian-Super-Fish) | $R=6.04275$ (I assumed Ciprian value) |
| Power Dissipated(kW) | $V_1^2/r=1.48$ | $V_1^2/r=1.48$ |
| | $V_2^2/r=1.1046$ | $V_2^2/r=1.22$ |
| | $V_3^2/r=0.7833$ | $V_3^2/r=1.10$ |
| | $V_4^2/r=0.4781$ | |

$$E_z = M \sin(\omega t + \varphi - k_z z) I_0(k_t r)$$

$$M = (3 \times 3^{0.5} / 2\pi) E_{zef}$$

E_{zef} is used in GPT simulation

Typical value for E_{zef} in our simulation is about 4.4×10^6 V/m.

Which means $M = 3.6 \times 10^6$ V/m and therefore $E_{z_axial} = M = 3.6 \times 10^6$ V/m.

With a gap of $g = 21.5$ mm, we will have

$$V_{axial} = Eg = 77.400 \text{ kV!}$$

Is transit time factor missing ?

Is the transit time factor about $160/260 = 0.61$?

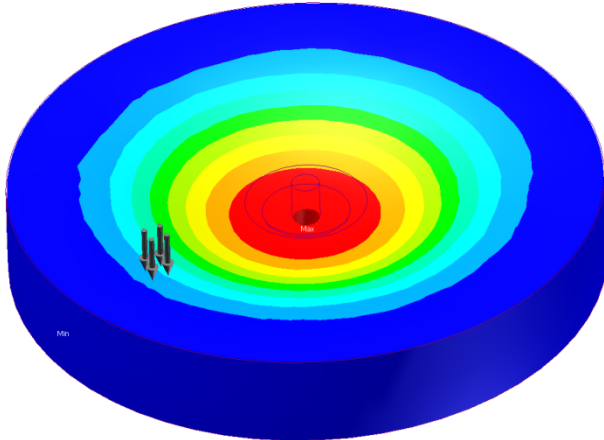
There is a factor of 2 roughly missing between the 160 kV from EM simulation and 77.4 kV from GPT. Has this anything to do with different definitions, for example linac definition for p :

$$p = V_1^2 / 2r$$

Effect of vacuum loading on MEBT rebunching cavity

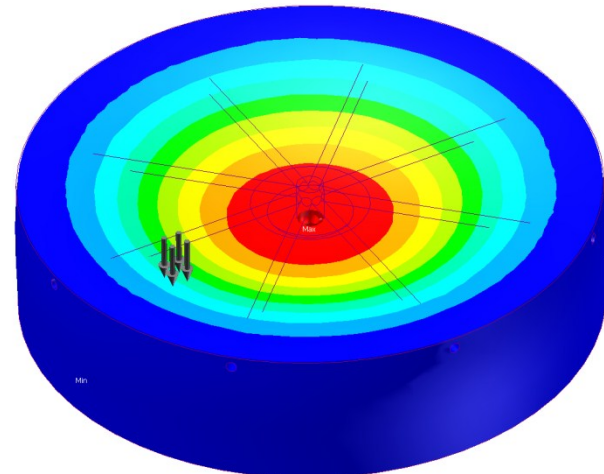
72mm inner rad
Cooling channels NOT present
Wall thickness = 25mm
Pressure = 100,000 Pa
Material: Copper
Max equivalent stress = 5.2MPa
Safety Factor = 15
Maximum deformation = 0.035mm

Deformation
Type: Deformation
Unit: mm
10/01/2013 14:45
0.035187 Max
0.031278
0.027366
0.023458
0.019546
0.015639
0.011729
0.0078194
0.0039097
0 Min



20mm inner rad
Cooling channels present
Wall thickness = 25mm
Pressure = 100,000 Pa
Material: Copper
Max equivalent stress = 7.7MPa
Safety Factor = 15
Maximum deformation = 0.07mm

Deformation
Type: Deformation
Unit: mm
10/01/2013 14:39
0.072724 Max
0.064643
0.056563
0.048483
0.040402
0.032322
0.024241
0.016161
0.0080804
0 Min



Conclusion:

Nose to nose gap will reduce from 16mm by approx 0.14mm

Inner volume will reduce by a small amount

Should not reduce wall thickness below 25mm. The deformation is not very significant

Thank you