



Science & Technology  
Facilities Council

# **TS1 Target Upgrade**

**Dan Wilcox**

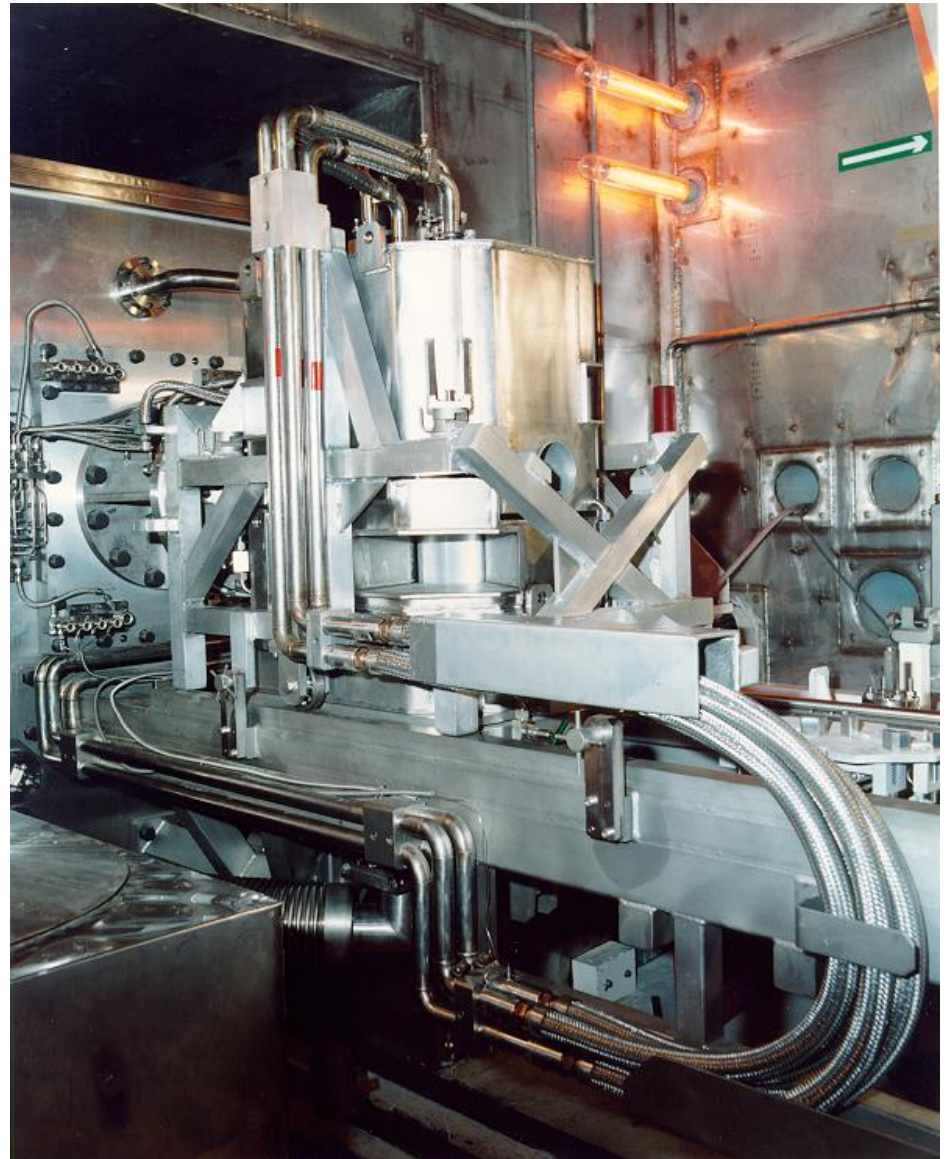
**High Power Targets Group**

**PASI Targets Meeting**

**05/12/2013**

# Overview

- Background / Aims
- Target Design
  - Target Concepts: optimising for neutronics
  - Design 1: Parallel Flow
  - Design 2: Series Flow
  - Initial FEA Modelling
  - Extra neutronic gains
- Increasing Beam Power
  - Engineering
  - Neutronics
- Conclusions

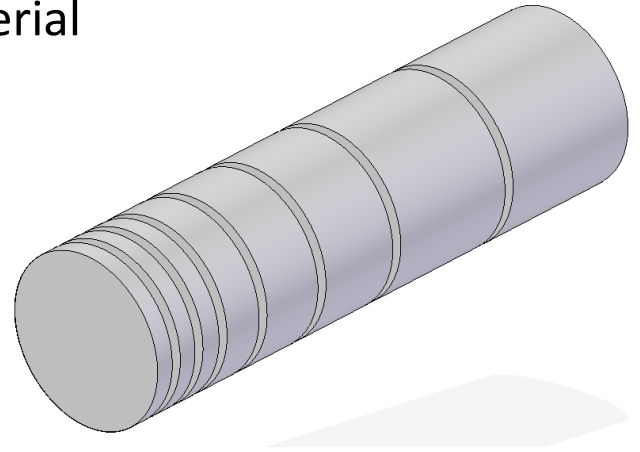


# Aims

- Increase the useful neutronic output of TS1
  - Use knowledge, experience and modern computational tools to optimise output from existing beam
  - Upgrade accelerator to deliver higher beam powers
- PASI WP2:
  - Detailed design for up to 0.5MW (625 $\mu$ A at 800MeV)
  - Conceptual target design for 1MW and 5MW
- TS1 Upgrade Project:
  - Increase useful neutronic output as much as possible, with low operational risk, on a limited budget, for implementation by  $\approx$ 2020

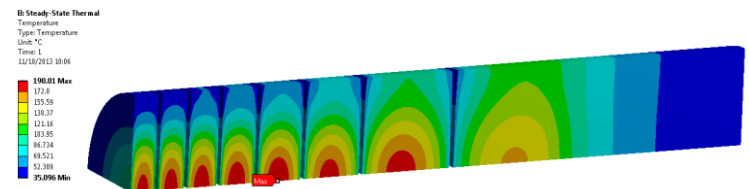
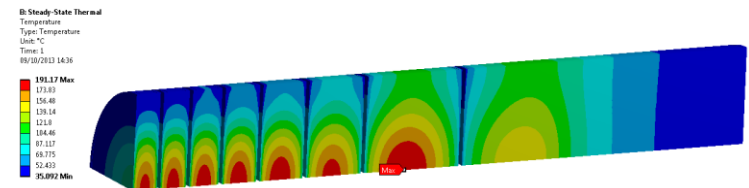
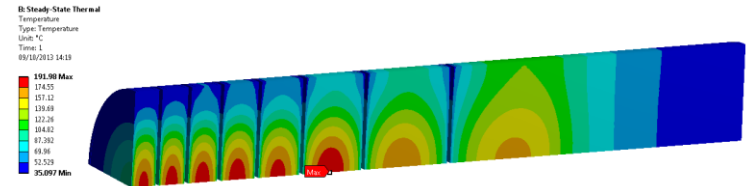
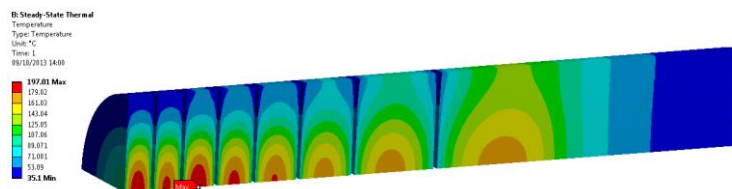
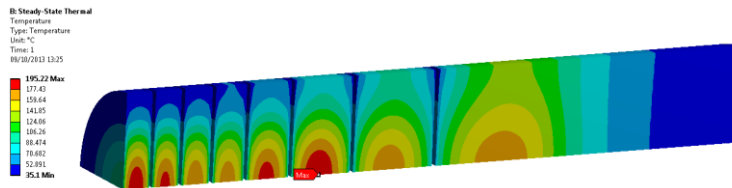
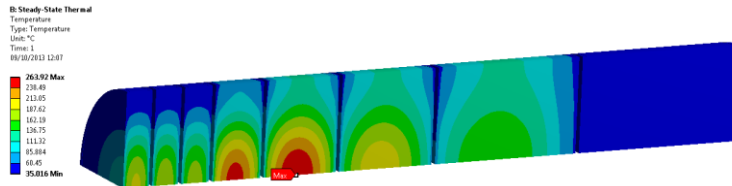
# Target Concepts

- For 180 - 625 $\mu$ A we need a plate target
  - Thermal stress limits solid rod targets to <60 $\mu$ A
  - Cannelloni targets are not neutronicly worthwhile until  $\approx$ 1MW (too much water)
- Minimise volume of water and non-target material
  - Water anywhere is bad for pulse width
- Circular cross section is best for neutronics
- Leave space for a water pre-moderator
- Avoid stainless steel – it generates a high neutron background
- Neutronic design order is; reflectors, then moderators, then pre-mod, then target



# Plate Thickness Optimisation

- Regardless of target shape, it is important to minimise the number of plates used
  - More plate gaps = more water and tantalum
- Current TS1 has high stress in plates 1 and 2, but not in 3-12
  - Use FEA to optimise the stress distribution across all plates
  - Do not exceed the stress limits in current TS1 (we know it works!)



# Plate Thickness Optimisation

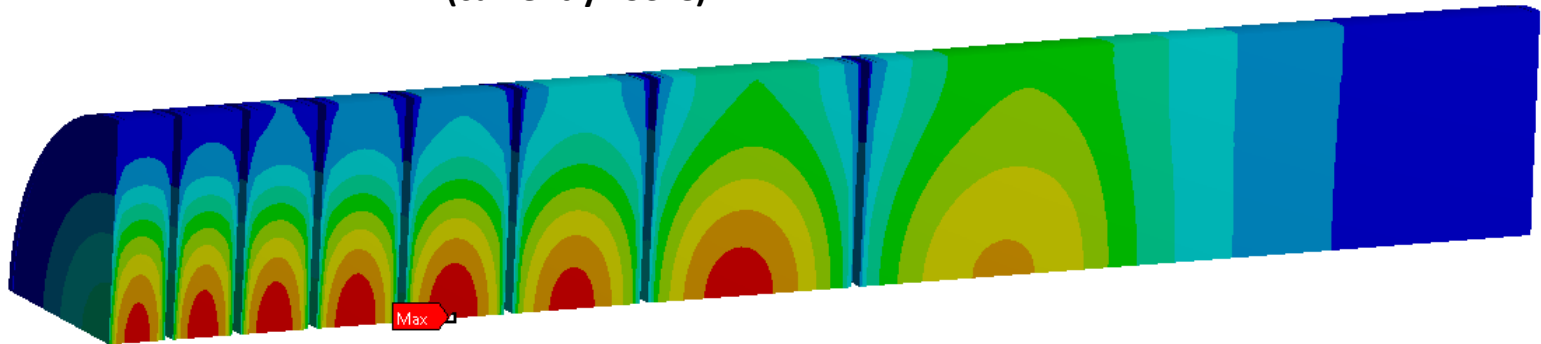
- Result: 8 plates required at 180 $\mu$ A

## B: Steady-State Thermal

Temperature  
Type: Temperature  
Unit: °C  
Time: 1  
11/10/2013 11:22

Maximum core temperature = 190°C  
(currently 193°C)

190.01 Max  
172.8  
155.59  
138.37  
121.16  
103.95  
86.734  
69.521  
52.309  
35.096 Min

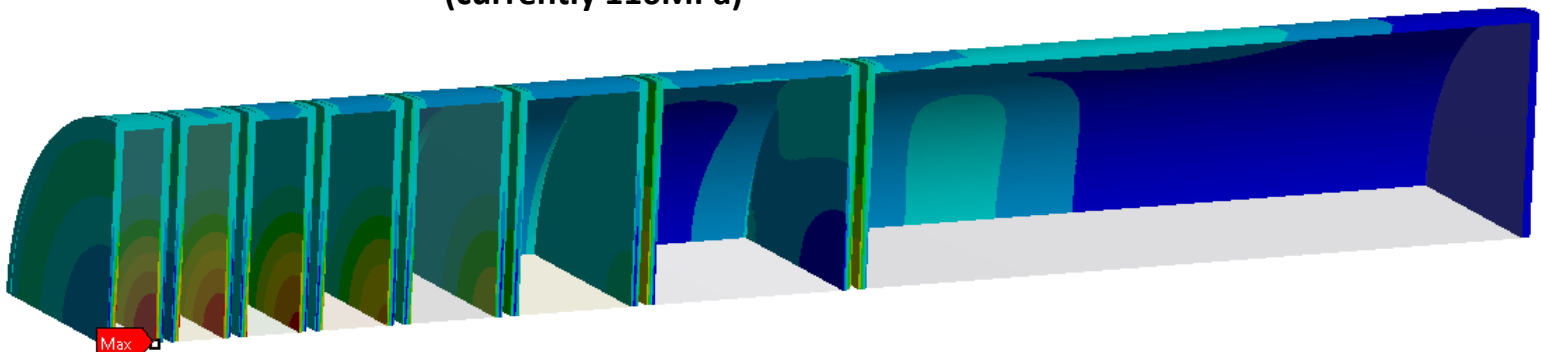


## C: Static Structural

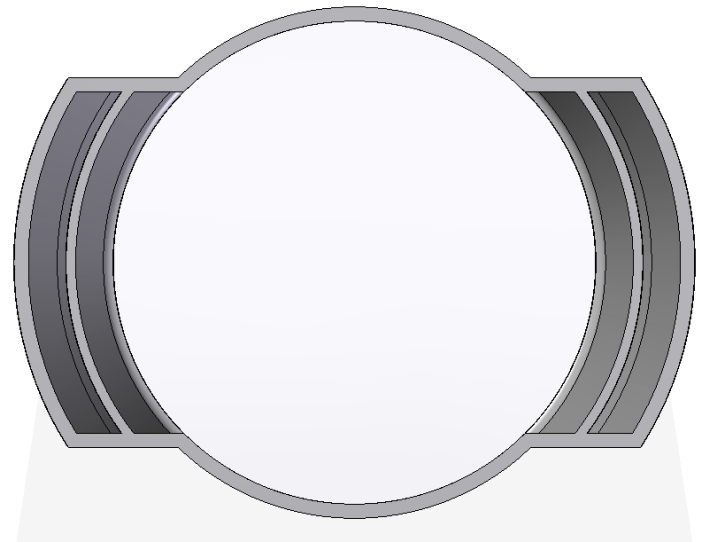
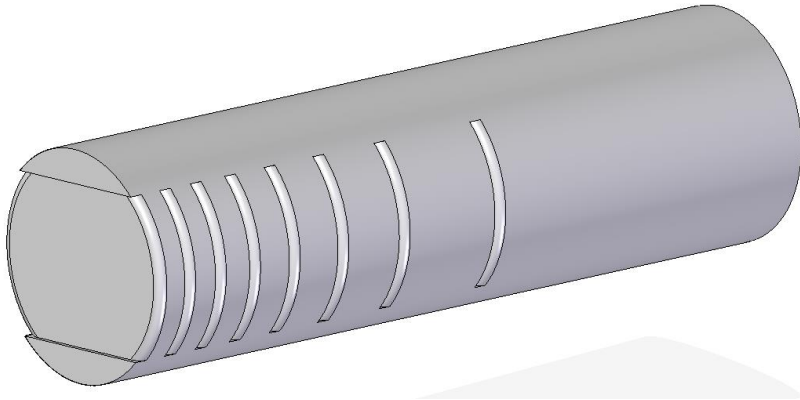
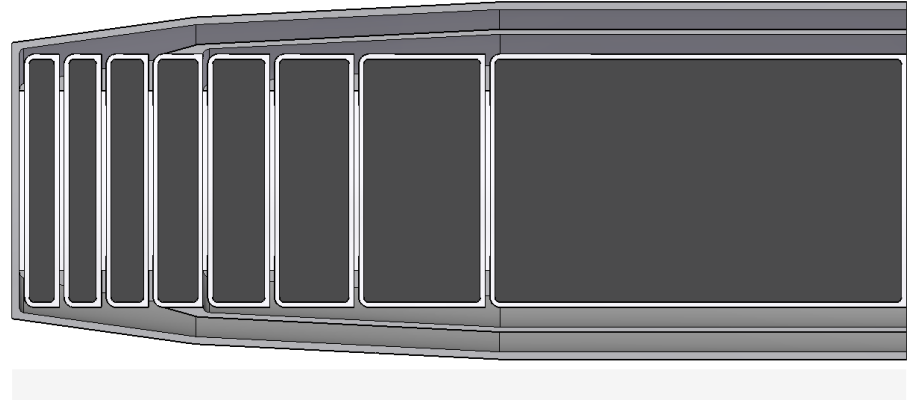
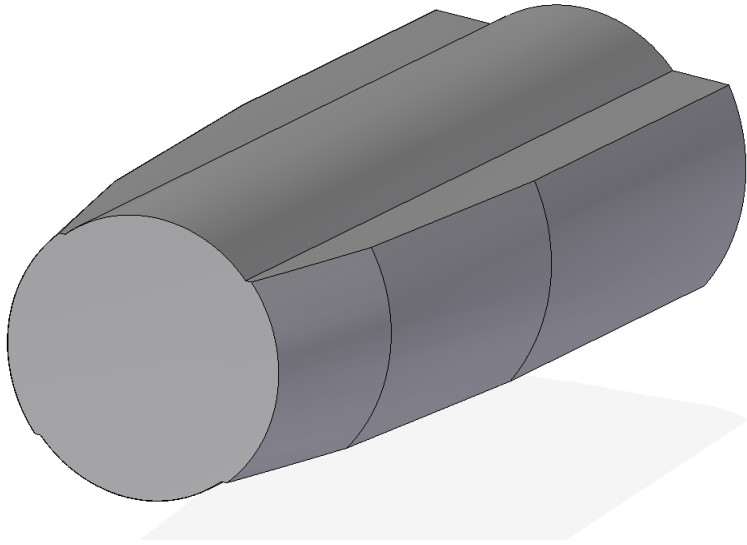
Equivalent (von-Mises) Stress - DomainTa  
Type: Equivalent (von-Mises) Stress  
Unit: Pa  
Time: 1  
11/10/2013 11:23

Maximum stress in Tantalum = 106MPa  
(currently 116MPa)

1.0582e8 Max  
9.4072e7  
8.2323e7  
7.0575e7  
5.8827e7  
4.7079e7  
3.5331e7  
2.3583e7  
1.1835e7  
86692 Min

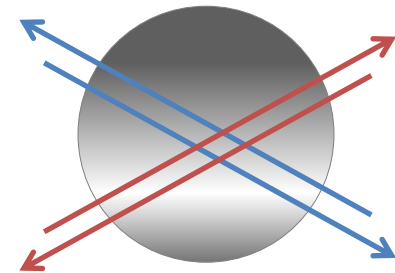
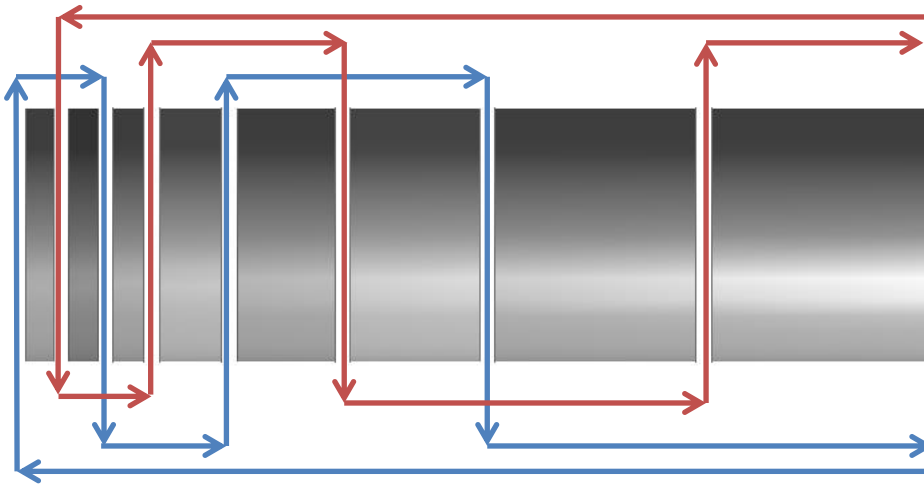


## Target Design 1: Parallel Flow



## Target Design 2: Series Flow

- Can reduce water volume further by having one water channel cross several plates – ‘series flow’
- A 2 channel scheme is proposed:

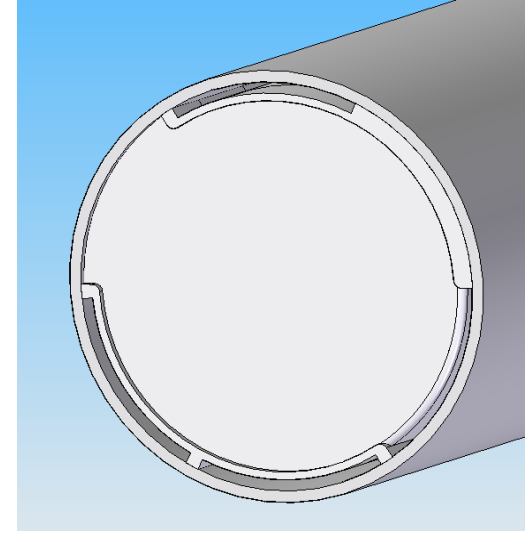
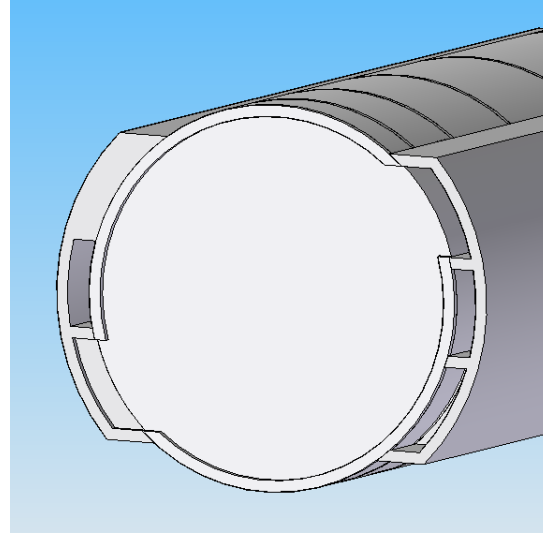
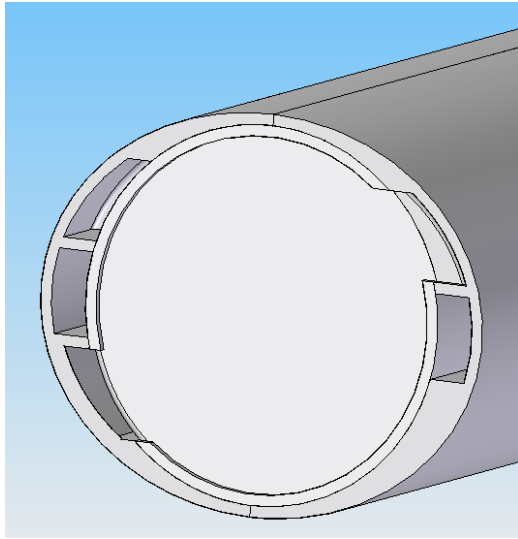


- Every plate is cooled by both channels
- Less face coverage, but channels are offset diagonally
- Lower flowrate, higher pressure drop



## Target Design 2: Series Flow

- There are several options for cross section geometry:

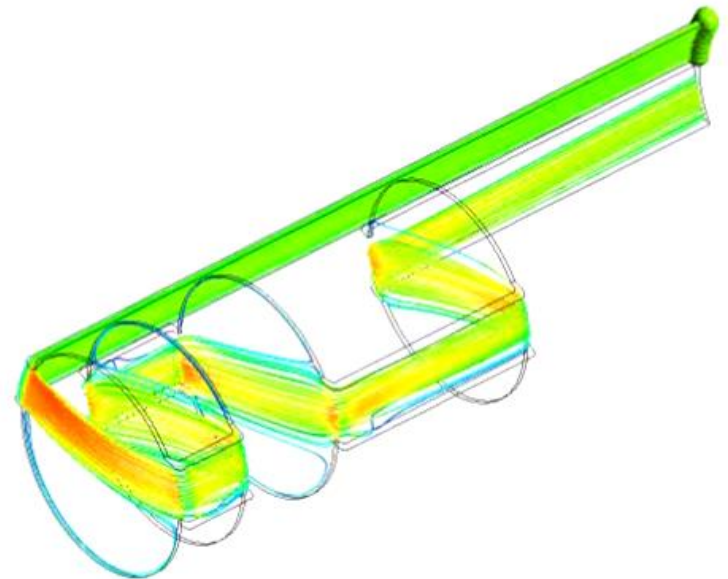
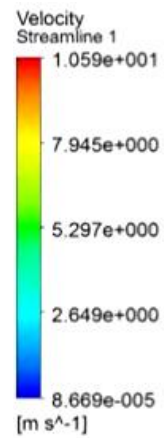
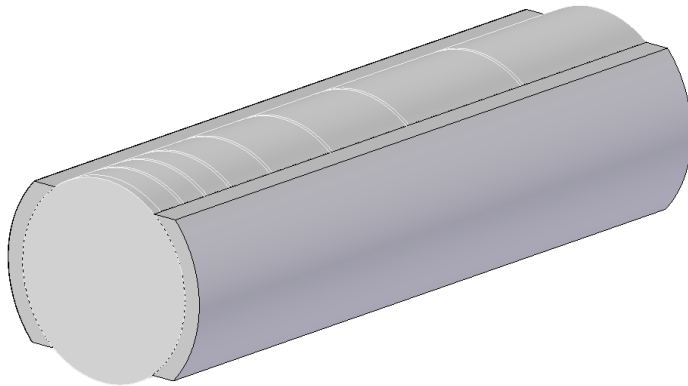
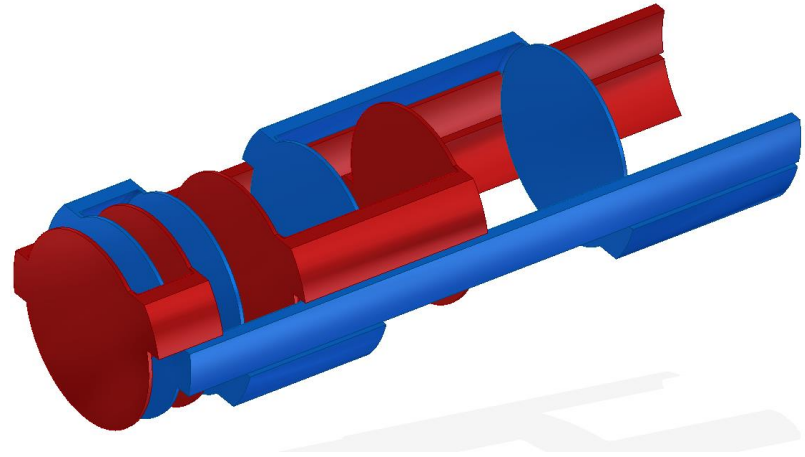
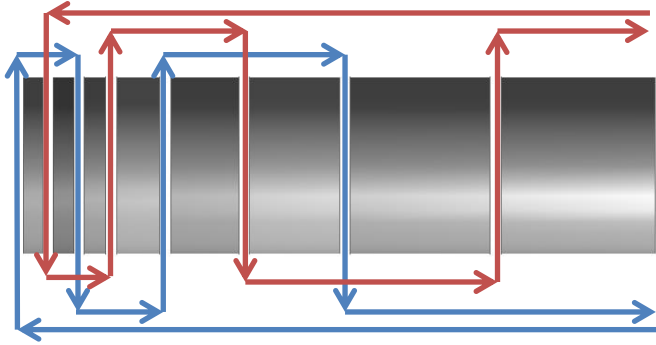


Better Neutronics

Easier Manufacture

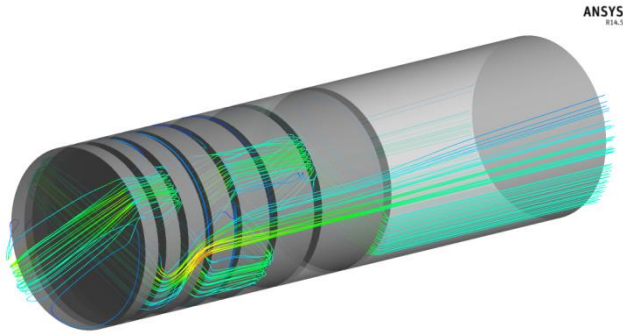
- There are also various options for plate face cooling
- Optimisation of cooling flow is still in progress

## Target Design 2: Series Flow

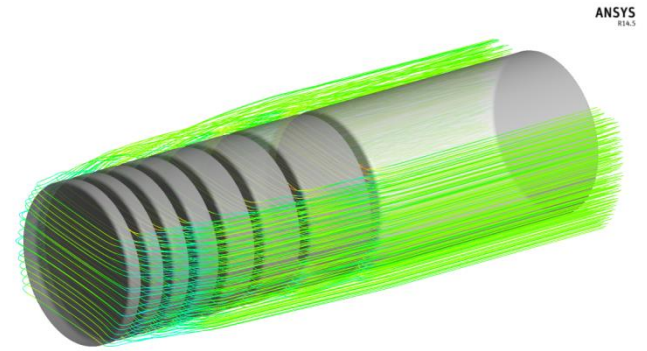


# Initial FEA Modelling

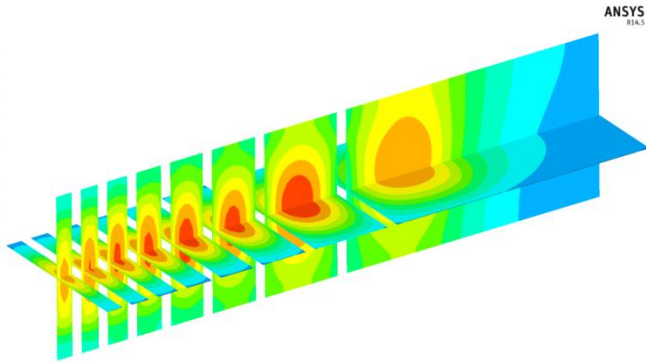
Velocity  
Streamline 1  
2.821e+001  
2.116e+001  
1.411e+001  
7.053e+000  
1.642e-004  
[m s<sup>-1</sup>]



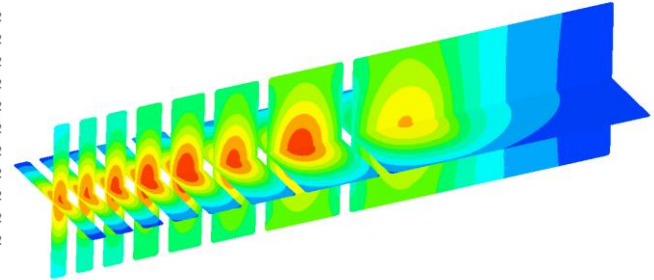
Velocity  
Streamline 2  
1.585e+001  
1.194e+001  
8.034e+000  
4.125e+000  
2.157e-001  
[m s<sup>-1</sup>]



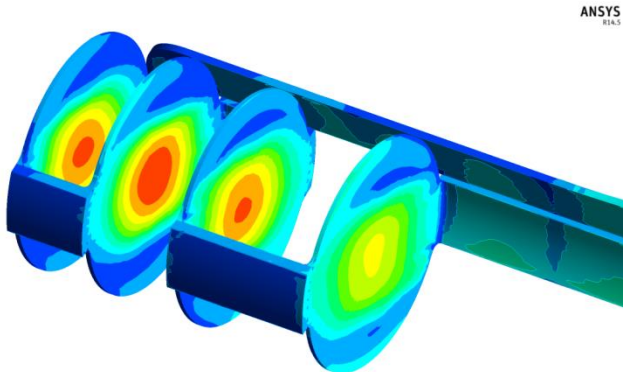
Temperature  
Contour 1  
4.855e+002  
4.678e+002  
4.500e+002  
4.323e+002  
4.146e+002  
3.968e+002  
3.791e+002  
3.614e+002  
3.436e+002  
3.259e+002  
3.081e+002  
[K]



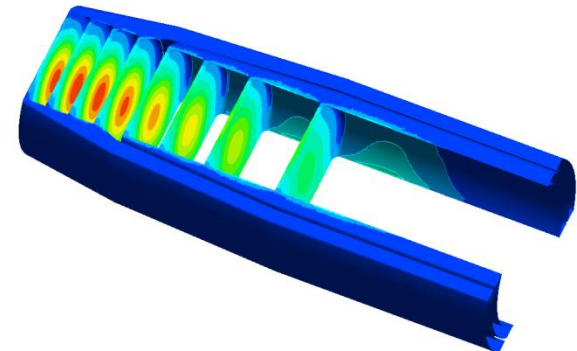
Temperature  
Contour Temp  
4.632e+002  
4.477e+002  
4.322e+002  
4.167e+002  
4.012e+002  
3.857e+002  
3.702e+002  
3.547e+002  
3.392e+002  
3.237e+002  
3.081e+002  
[K]



Heat Flux  
Contour 6  
2.356e+006  
2.110e+006  
1.863e+006  
1.616e+006  
1.370e+006  
1.123e+006  
8.764e+005  
6.297e+005  
3.830e+005  
1.363e+005  
-1.104e+005  
[W m<sup>-2</sup>]



Heat Flux  
Contour 2  
2.174e+006  
1.956e+006  
1.737e+006  
1.519e+006  
1.300e+006  
1.081e+006  
8.626e+005  
6.439e+005  
4.253e+005  
2.066e+005  
-1.200e+004  
[W m<sup>-2</sup>]



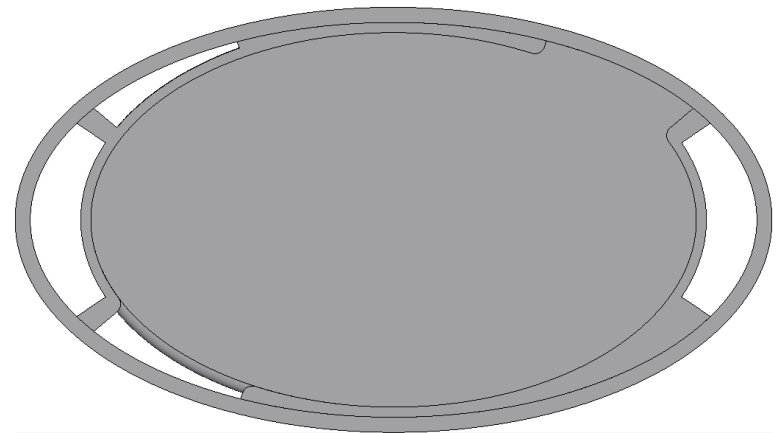
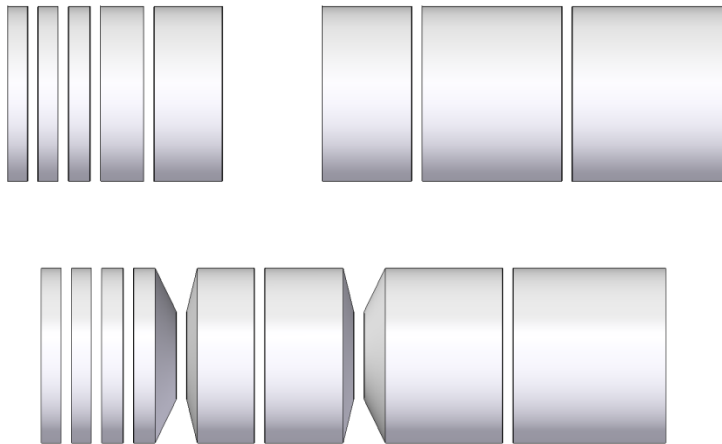
# Comparison

	Series Flow (9m/s)	Parallel Flow (6m/s)
Max core temp (°C)	212	205
Max surface temp (°C)	170	132
Max heat flux (MW/m <sup>2</sup> )	2.4	2.1
Max pressure drop (bar)	5.0	0.3
Water mass flow rate (kg/s)	1.6	8.0
Total water volume (cm <sup>3</sup> )	250	840

- Series flow target has higher temperatures (but within acceptable limits)
- Heat flux is acceptable in both targets
- Series flow target has much higher pressure drop, but lower flow rate
- Parallel flow target has a significantly higher volume of water

# Extra Neutronic Gains

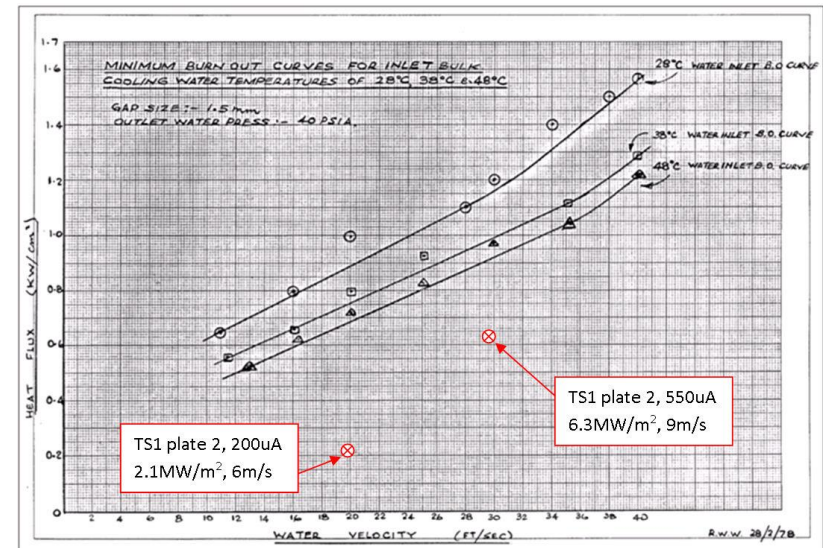
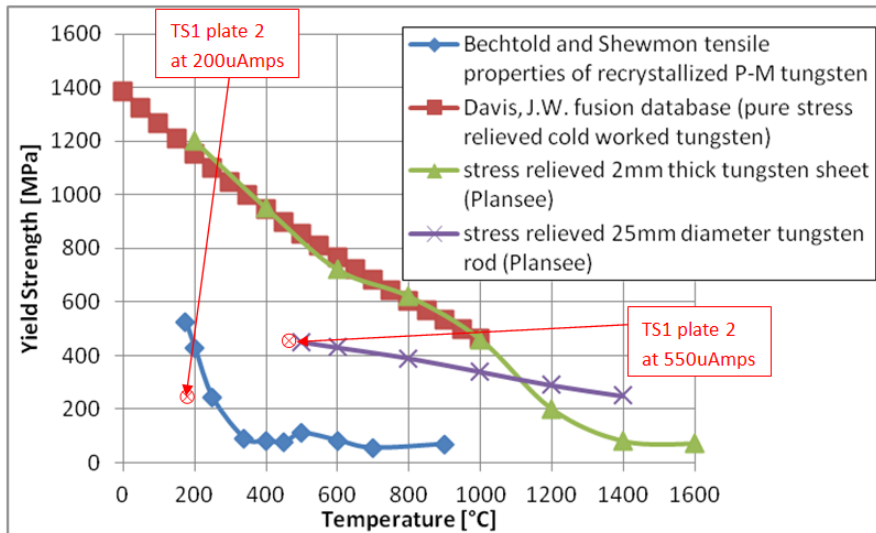
- Can add a flux trap to get more neutrons out
- Can use a horizontally elliptical beam – wider area seen by the moderators



- ... but these options will also increase manufacturing cost and complexity
- Further engineering design and neutronic modelling will help quantify the costs and benefits

# Increasing Beam Power – Engineering

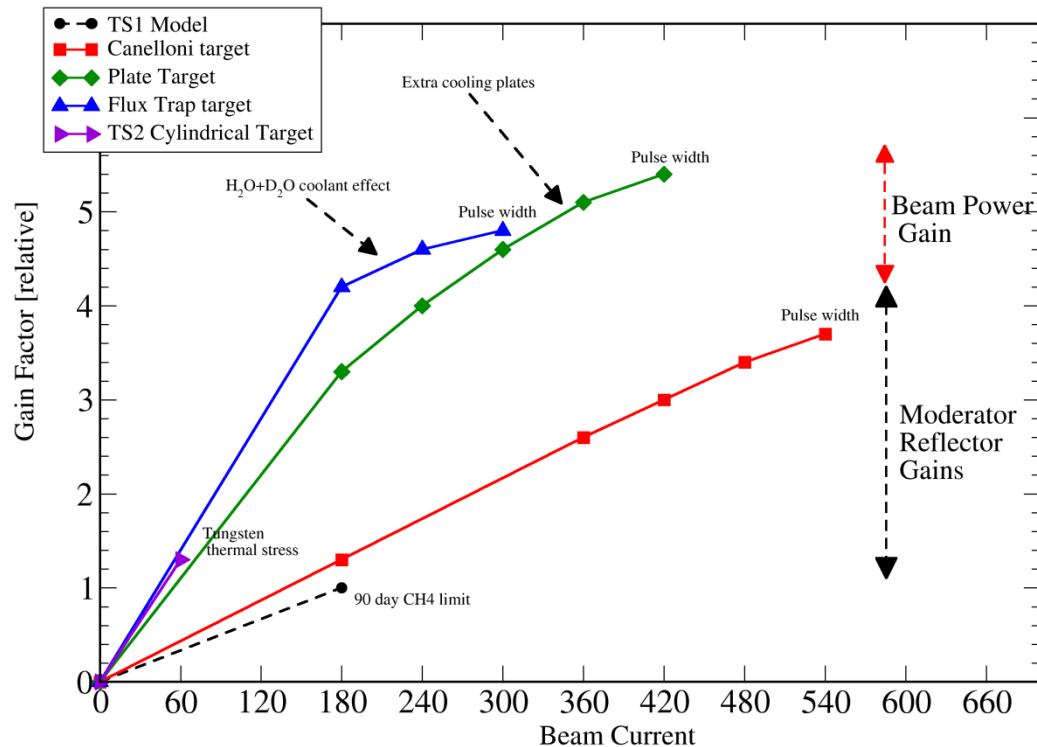
- Tristan Davenne modelled plate 2 of the current target at 200 and 550 $\mu$ A



- At 550 $\mu$ A:
  - Heat flux exceeds ISIS design limits: still below burnout curve, but lower factor of safety. May need to increase water pressure to prevent boiling.
  - Tungsten may exceed its yield stress (according to some sources). ISIS design limit is 275MPa.
  - Tantalum stress appears to depend more on HIP pre-stress than beam heating – this will be validated using pre-stress measurements from ENGIN-X

# Increasing Beam Power – Neutronics

- Stuart Ansell and Goran Skoro modelled neutronic gain as a function of beam current for several target types:



- Higher beam power => more plates required => more water in target => longer neutron pulse width

# Increasing Beam Power

- For neutronics, plate targets are undesirable at above  $\approx 420\mu\text{A}$
- This limit could be raised by reducing the number of target plates used at a given beam power – but go too far and reliability will be compromised
- The current beam window can only withstand  $\approx 300\mu\text{A}$ ; this will probably be the limiting factor for first upgrade
- At 1MW and above, a radically different target design will be required
  - SINQ uses a cannelloni target at 1MW – but as a pulsed source, ISIS may have problems with thermal shock and neutron pulse width
  - SNS second target station will be 1MW long pulse, rotating tungsten and liquid mercury targets under consideration



# Conclusions

- The coming TS1 upgrade will require a target to operate at 200-300 $\mu$ A
- Parallel flow target is a conservative baseline
  - Significantly better neutronic performance without compromising reliability
- Series flow target should be neutronically better, if it is worthwhile from an engineering/manufacturing perspective
- Both designs can be adapted to include a flux trap and/or elliptical plates, if this is found to be worthwhile
- Parallel flow target should be suitable at 500 $\mu$ A or more, however...
  - Limited by neutronics at  $\approx$ 420 $\mu$ A
  - Limited by beam window at 300 $\mu$ A
- At 1MW+ plate targets are no longer suitable and a completely new target design will be required